

INITIAL INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

EXISTING CCR IMPOUNDMENTS
CCR Rule Section 257.82

ASBURY POWER PLANT

21133 Uphill Lane
Asbury, Missouri 64832

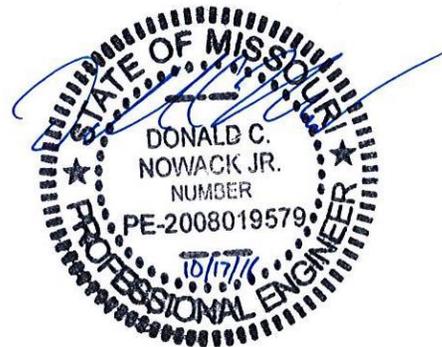
October 17, 2016



SERVICES YOU COUNT ON

EMPIRE DISTRICT ELECTRIC COMPANY

Prepared by:



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October 17, 2016

Empire District Electric Company
Asbury Power Plant
21133 Uphill Lane
Asbury, Missouri 64832

RE: Initial Inflow Design Flood Control System Plan . CCR Rule Section 257.82
Empire District Electric Company . Asbury Power Plant
Asbury, Missouri
PPI Project Number 231518

To Whom It May Concern:

This document presents the **Initial Inflow Design Flood Control System Plan** for the Empire District Electric Company's CCR Impoundment at the Asbury Power Plant. This document has been prepared to meet the requirements of Section 257.82 of the CCR Rule.

In accordance with Section 257.105(g)(4), a copy of this document should be placed in Empire's operating record. In accordance with Section 257.107(g)(4), this document should also be posted to Empire's CCR Compliance website. Notification of the availability of this document should be provided to the State Director, as required in Section 257.106(g)(4).

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INITIAL INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN – EXISTING CCR IMPOUNDMENTS

CCR RULE SECTION 257.82

EMPIRE DISTRICT ELECTRIC COMPANY – ASBURY POWER PLANT

ASBURY, MISSOURI

1.0 INTRODUCTION

This Initial Inflow Design Flood Control System Plan has been prepared according to the U. S. Environmental Protection Agency final rule regarding the disposal of coal combustion residuals from electric utilities (40 CFR Part 257 and 261, also known as the CCR Rule). The CCR Rule Section 257.82 requires the owner or operator of an existing or new CCR surface impoundment or any lateral expansion of a CCR surface impoundment must design, construct, operate, and maintain an inflow design flood control system according to the requirements of this Section.

This plan may be amended at any time provided the revised plan is placed in the facility's operating record as required by Section 257.105(g)(4). This plan must be amended whenever there is a substantial change in conditions or a minimum of every five (5) years.

The Asbury Power Plant maintains one CCR impoundment, the Asbury CCR Impoundment. The Impoundment accepts all CCR wastes generated by the Asbury Power Plant. See Figures 1 and 2 in Appendix I for the Asbury CCR Impoundment location on a topographic map and aerial photograph, respectively.

The Asbury CCR Impoundment is subdivided into three (3) operational Ponds, identified as the Lower Pond, Upper Pond, and South Pond. The Lower Pond, Upper Pond, and South Pond are separated by interior earthen embankments. The Upper Pond is further subdivided by an interior dike into Upper Pond A (North Cell of the Upper Pond) and Upper Pond B (South Cell of the Upper Pond). The Lower Pond is further subdivided by interior dikes into several sections. The sections of the Lower Pond are identified as Sections D through J for the purposes of this Report. See Figure 3 in Appendix I for a diagram showing each section located within the Asbury CCR Impoundment.

The following sections of this report assess the hydrologic and hydraulic capacity requirements for the Asbury CCR Impoundment.

2.0 ANALYSIS OF EXISTING INFLOW DESIGN FLOOD CONTROL SYSTEM

2.1 Hazard Classification and Design Assumptions

The Asbury CCR Impoundment is classified as a significant hazard potential CCR surface impoundment in accordance with Section 257.73(a)(2) of the CCR Rule. In accordance with Section 257.82(a), the inflow design flood control system must adequately manage flow for a 1,000-year flood.

Design assumptions for the hydrologic and hydraulic model include the following:

1. There is virtually no loss of water through the bottom of the impoundment. Additionally, all sections of the Impoundment and drainage areas outside of the impoundment are modeled as impervious (CN = 98), with the exception of Lower Pond Section J, which has a significant amount of area that is not subject to submersion. The area within Lower Pond Section J that is not subject to submersion was assigned a CN number of 78 for meadow in good condition with hydrologic soil group D. These assumptions are considered conservative.
2. Three (3) sections within the Asbury CCR Impoundment normally operate with pools of water. The operating water levels used in the model for the Upper Pond A, Upper Pond B, and Lower Pond Section J are 952.5 feet, 953.6 feet, and 928.8 feet, respectively.
3. Process water entering the Asbury CCR Impoundment comes from three (3) sources: the coal pile sump, bottom ash sluice water discharge, and the Foggy Pond discharge.

Rainfall infiltrating the coal pile flows into a sump and is pumped into Upper Pond A.

Water in the Foggy Pond consists of process water and rain that falls within the small drainage area around the Pond. Foggy Pond is pumped into Upper Pond B when it fills during a precipitation event. For the model, all runoff from the Foggy Pond drainage area is pumped into Upper Pond B. In reality, the volume of water discharged from the Foggy Pond is limited by the pump capacity.

Bottom ash sluice water is pumped into Lower Pond Section G. Under normal operating conditions, makeup water for bottom ash sluice is obtained from Upper Pond B. To be conservative, the model does not account for water removal from Upper Pond B. Based on the bottom ash sluice pumps maximum capacity of 1625 gallons per minute and the pumping frequency of 3 hours per day, the 24 hour estimated maximum volume of bottom ash sluice water entering Lower Pond Section G is 0.90 acre-feet.

4. The National Weather Service Precipitation Frequency Data Server was used to determine the 1000 year recurrence interval precipitation estimate for the site. The 1,000 year event for the durations of 6 hours, 12 hours, and 24 hours were evaluated. The 24 hour, 1,000 year recurrence interval precipitation event was determined to be the critical design event that produced the maximum peak discharge for the system. For the 24 hour duration the precipitation depth is estimated at 13.6 inches. A copy of the output from the National Weather Service Precipitation Frequency Data Server is included in Appendix II.

With the exception of rainfall over the drainage areas at the coal pile and around the Foggy Pond, the inflow design flood for the Asbury CCR Impoundment is limited to the direct precipitation that falls within the perimeter of the Impoundment. Runoff pumped from the coal pile sump and the Foggy Pond is discharged into the CCR Impoundment in Upper Pond A and Upper Pond B, respectively.

Figure 3 in Appendix I is a diagram showing each section located within the Asbury CCR Impoundment, the approximate location of the drainage area for each section, and flow routing.

2.2 Hydrologic and Hydraulic Model

The volumes of the individual basins located within the Asbury CCR Impoundment were estimated using a 1-foot topographic map of the impoundment. The topographic map was developed from a comprehensive topographic survey performed in 2012. The topographic survey was updated in 2014, and again in August 2016. The August 2016 topographic survey update included surveying of areas in the Lower Pond where additional CCR had been placed, and surveying of the bottom of the South Pond.

See Figure 3 in Appendix I for a diagram showing each section located within the Asbury CCR Impoundment, the current topographic contours, the approximate location of the drainage area for each section, and flow routing. The following table provides the model input data used for each section.

| Section | Drainage Area (Acres) | Receives Water From | Lowest Elevation on Dike | TR55 CN |
|------------------------|------------------------------|----------------------------|---------------------------------|----------------|
| Upper Pond A | 4.94 | Coal Pile Sump | 953.8 | 98 |
| Upper Pond B | 14.87 | Foggy Pond | 954.4 | 93.42 |
| South Pond (Section C) | 12.40 | NA | 954.2 | 98 |
| Lower Pond Section D | 10.50 | Upper Pond A | 951.7 | 98 |
| Lower Pond Section E | 7.02 | Section D | 947.3 | 98 |
| Lower Pond Section F | 3.99 | NA | 952.8 | 98 |
| Lower Pond Section G | 4.39 | Bottom Ash Sluice | 946.9 | 98 |
| Lower Pond Section H | 9.51 | NA | 946.5 | 98 |
| Lower Pond Section I | 12.19 | NA | 944.4 | 98 |
| Lower Pond Section J | 39.30 | Upper Pond B | 931.5 | 86.61 |
| Coal Pile | 19.14 | NA | NA | 98 |
| Foggy Pond | 0.89 | NA | NA | 98 |

The U.S. Army Corps of Engineers HEC-1 software was used to model the flow of water through the connected sections within the impoundment and to estimate the ponding water level in isolated sections within the impoundment. The HEC-1 model is designed to simulate the surface runoff response of a watershed to precipitation by representing the watershed as an interconnected system of hydrologic and hydraulic components. Rainfall over the Asbury CCR Impoundment was modeled using the SCS Unit

Hydrograph method. The SCS Type II distribution and abstractions from rainfall were estimated using the NRCS Technical Release 55, Urban Hydrology for Small Watersheds. To be conservative, most of the drainage areas in the model were considered virtually impervious (CN = 98). The exception is Lower Pond Section J, which has a significant area that is not subject to submersion. With the exception of pumped flows from the coal pile and the small area around Foggy Pond, the Asbury CCR Impoundment is not subject to stormwater run-on from outside areas.

Seven (7) different HEC-1 models were developed based on the hydraulic connections within the Impoundment, which as summarized below.

- 1. Upper Pond A, Lower Pond Section D, and Lower Pond Section E:** The drainage area for Upper Pond A also includes the coal pile drainage area. The initial water level in Upper Pond A is 952.5 feet. Water discharges from Upper Pond A into Lower Pond Section D from three (3) 10-inch pipes. The intake of two of these pipes is set at 952.16 feet and the intake of the third pipe is set at 953.0 feet. Flow through these three pipes was estimated using Manning's equation. Water in Lower Pond Section D discharges to Lower Pond Section E from two (2) 10-inch pipes passing through the separating dike. Flow through these two pipes was estimated using Manning's equation until the pipe inlets became submerged with 2.5 feet of water. With water 2.5 feet or higher over the pipe inlets, flow was estimated using the Hazen Williams equation for flow under pressure. There are no external discharge spillways from Upper Pond A, Lower Section D, or Lower Pond Section E.
- 2. South Pond (Section C):** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There is no external discharge spillway on the perimeter levee embankment of the South Pond (Section C).
- 3. Lower Pond Section F:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There are no external discharge spillways from Lower Pond Section F.
- 4. Lower Pond Section G:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There are overflow pipes from Lower Pond Section G to Lower Pond Section J, but the ponding level in Lower Pond Section G does not reach the pipe inverts under the design flood. There is no external discharge spillway from Lower Pond Section G.
- 5. Lower Pond Section H:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There is no external discharge spillway from Lower Pond Section H.

6. **Lower Pond Section I:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There is no external discharge spillway from Lower Pond Section I.
7. **Upper Pond B and Lower Pond Section J:** The drainage area for Upper Pond B also includes the Foggy Pond drainage area. The initial water level in Upper Pond B was modeled as 953.6 feet. Water discharges from Upper Pond B into Lower Pond Section J from one (1) 10-inch pipe. The intake of this pipe is set at approximately 953.0 feet. Flow through this pipe was estimated using Manning's equation.

The initial water level in Lower Pond Section J is 928.8 feet. Water from Section J is discharged at Outfall #002 through a primary spillway consisting of two (2) 12-inch pipes. The intake of these two (2) pipes is set at approximately 928.8 feet. Flow through these pipes was estimated using Manning's equation.

Outfall #002 also has an auxiliary spillway consisting of a trapezoidal shaped concrete channel that is 24 feet wide and 1.2 feet from the bottom of the spillway to the top of the berm. The flowline of the auxiliary spillway is at elevation 930.35 feet. Flow over the auxiliary spillway was estimated using the equation for flow over an Ogee spillway.

2.3 Hydrologic and Hydraulic Modeling Results

Table 2.3-1 below summarizes the results of the modeled stormwater flooding event, including the resulting water elevation and freeboard in each basin.

| Section | Result of 1000 Year Rainfall | Computed Water Elevation (ft.) | Freeboard (feet) |
|------------------------|-------------------------------------|---------------------------------------|-------------------------|
| Upper Pond A | Flows into Section D | 953.45 | 0.35 |
| Upper Pond B | Flows into Section J | 954.14 | 0.26 |
| South Pond (Section C) | Contains Rainfall | 952.39 | 1.81 |
| Lower Pond Section D | Flows into Section E | 951.41 | 0.29 |
| Lower Pond Section E | Contains Rainfall | 946.61 | 0.69 |
| Lower Pond Section F | Contains Rainfall | 950.46 | 2.34 |
| Lower Pond Section G | Contains Rainfall | 941.79 ¹ | 5.11 |
| Lower Pond Section H | Contains Rainfall | 941.45 | 5.05 |
| Lower Pond Section I | Contains Rainfall | 939.20 | 5.2 |
| Lower Pond Section J | Contains Rainfall | 929.01 | 2.49 |

¹The computed water elevation for Section G includes 0.90 acre feet of water more than what was calculated in the HEC-1 model. The additional 0.90 acre-feet of water is the maximum daily discharge from pumping of bottom ash sluice water.

Lower Pond Section E, which is the end basin for flows from the coal pile, Upper Pond A, and Lower Pond Section D, contains the design flood with a freeboard of 0.69 feet below the lowest part of the exterior perimeter levee embankment.

South Pond (Section C) and Lower Pond Sections F, G, H, and I are relatively isolated from the other portions of the Impoundment and have sufficient storage volume to contain the precipitation within them without overflowing into an adjacent section. Freeboard in each of these basins is greater than one foot.

Lower Pond Section J, which is the end basin for flows from the Foggy Pond and Upper Pond B, contains the design flood with a freeboard of 2.49 feet below the lowest part of the dike and 1.34 feet below the auxiliary spillway. Note that Lower Pond Section J was modeled with the two (2) outlet pipes open during the storm event.

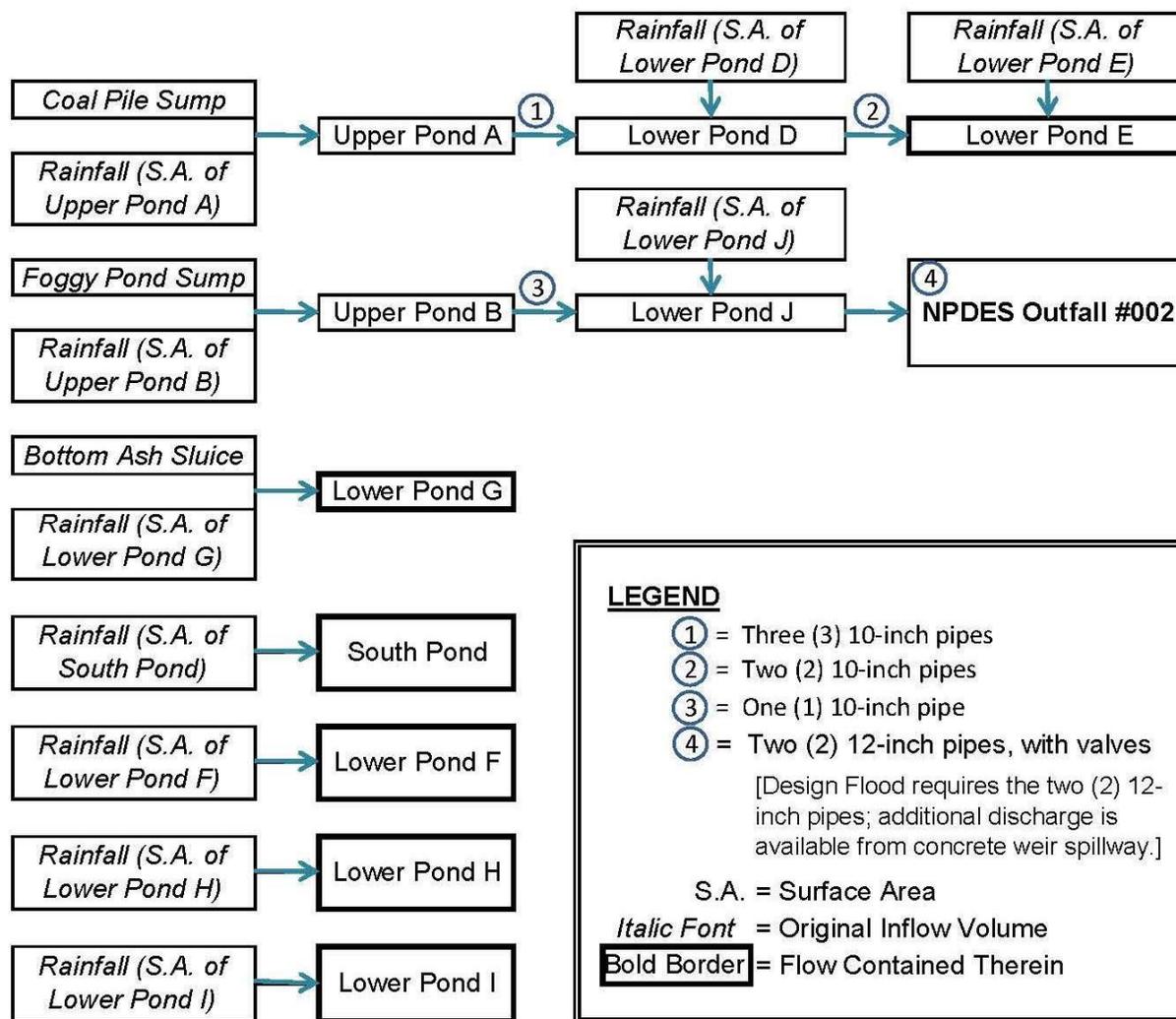
2.4 Conclusions

The Asbury CCR Impoundment is capable of adequately managing the Design Flood under existing conditions. The total capacity of the permitted discharge point, NPDES Outfall #002, exceeds what is necessary during the Design Flood event. In addition to the excess capacity of the spillway at NPDES Outfall #002, there is excess storm water storage capacity in several sections of the Impoundment. Empire has several options available to convey excess storm water by gravity flow or pump excess storm water if necessary.

3.0 INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

The Empire District Electric Company's Inflow Design Flood Control Plan for the Asbury CCR Impoundment is summarized in the flow chart below. Under typical operating conditions, the Design Flood event is discharged through the two (2) 12-inch outlet pipes in Section J of the Lower Pond, at NPDES Discharge #002.

INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN



3.1 Contingency Planning

The two (2) 12-inch outlet pipes are regularly observed by Empire staff to verify their functionality. In the event of unanticipated conditions, such as obstruction of one or more of these discharge pipes, or a storm event that exceeds the Design Flood event, Empire can make several different operational adjustments for routing of additional storm water. Some of these operational adjustments are summarized in the list below.

As previously stated, the Asbury CCR Impoundment passes the Design Flood event under normal operating conditions. The options listed below are presented for contingency planning purposes only and are not explicitly incorporated into the Inflow Design Flood Control System Plan.

1. Additional storm water flow capacity is available from the auxiliary concrete spillway at NPDES Outfall #002, in Lower Pond Section J.
2. Additional storm water storage is available in the South Pond (Section C). Water can be conveyed to the South Pond from Upper Pond B by opening of one or both of the two (2) 12-inch pipes with valves between Upper Pond B and the South Pond.
3. The bottom ash sluice pumps can be utilized to pump water from Upper Pond B to Section G of the Lower Pond.

4.0 CCR RULE SECTION 257.82(c)(5) – CERTIFICATION

The undersigned Professional Engineer certifies that the Inflow Design Flood Control System Plan meets the requirements of 40 CFR 257.82.

State of Missouri Professional Engineering License Number: 2008019579

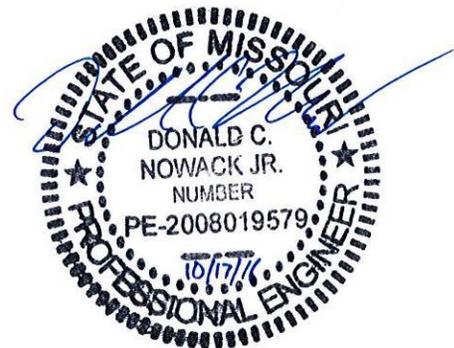
State of Missouri Professional Engineering License Number: 2008019579

Name: Donald C. Nowack, P.E.

Seal:

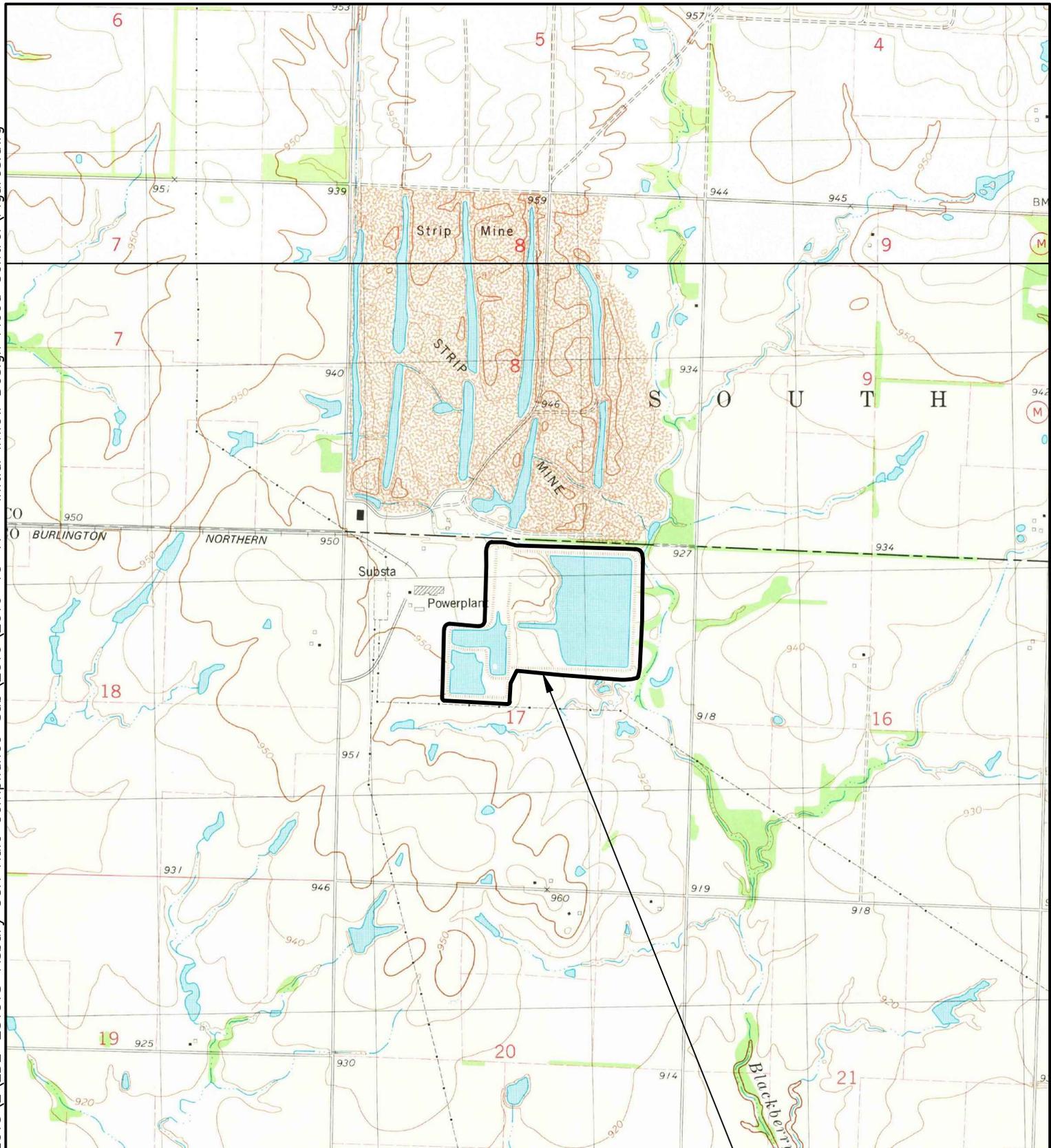
Signature: 

Date: October 17, 2016



APPENDIX I
FIGURES

S:_MASTER PROJECT FILE\2015\E\DE-231518-Asbury CCR Rule Compliance-Sub\2016\2016-10-17 - Initial Inflow Design Flood Control\Figures.dwg



USGS Asbury 7.5 Minute Topographic Quadrangle, 1981
 USGS Mindenmines 7.5 Minute Topographic Quadrangle, 1981

Asbury CCR Impoundment

Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, MO
 Client: Empire District Electric Company

Site Location on Topographic Map

DATE: October 17, 2016

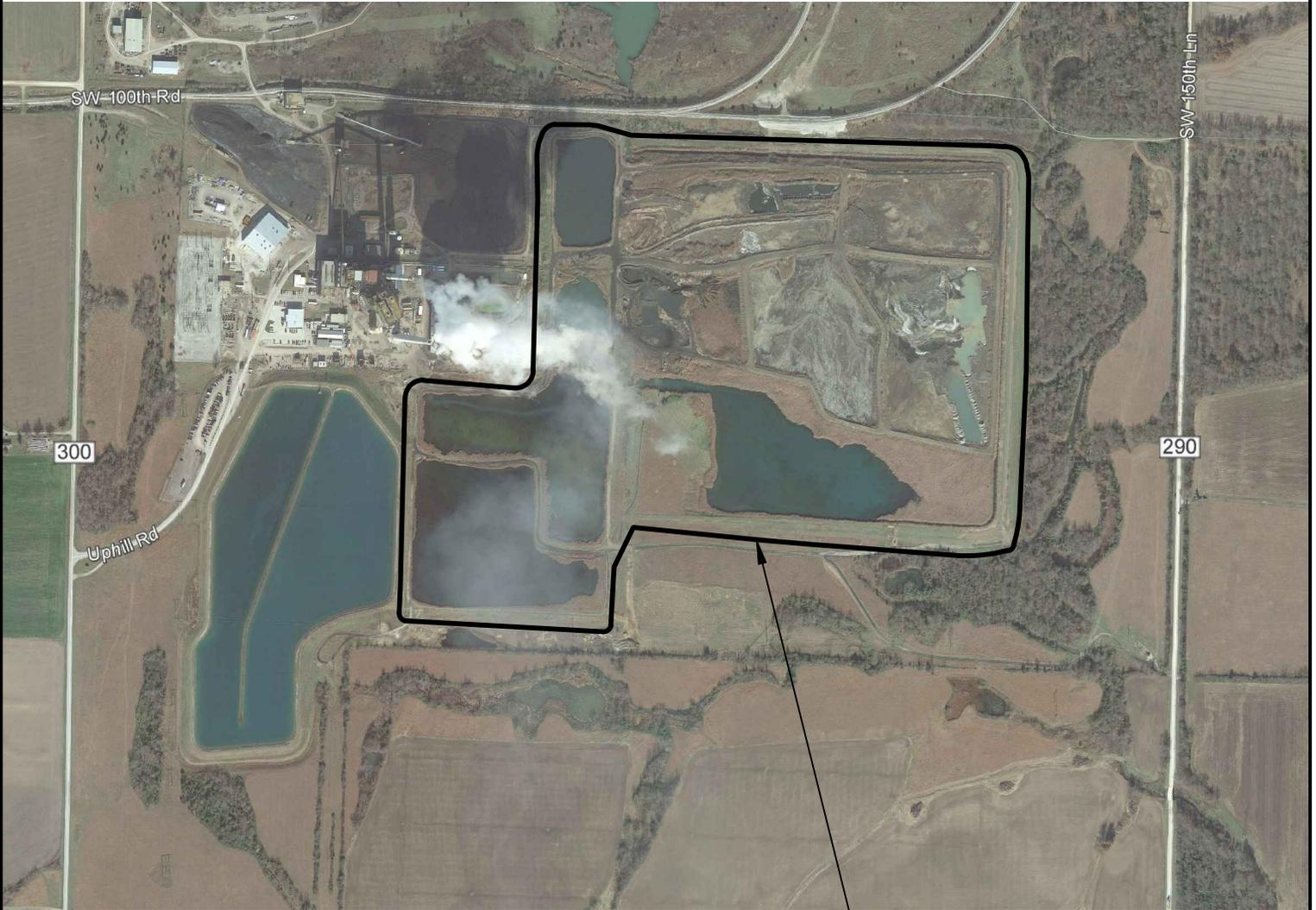
Project Number: 231518



SCALE
 1"=2000'

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 GEOTECHNICAL AND MATERIALS ENGINEERS/MATERIALS TESTING LABORATORIES/ENVIRONMENTAL SERVICES

FIGURE 1



Asbury CCR Impoundment



SCALE
1"=800'

Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, MO
Client: Empire District Electric Company

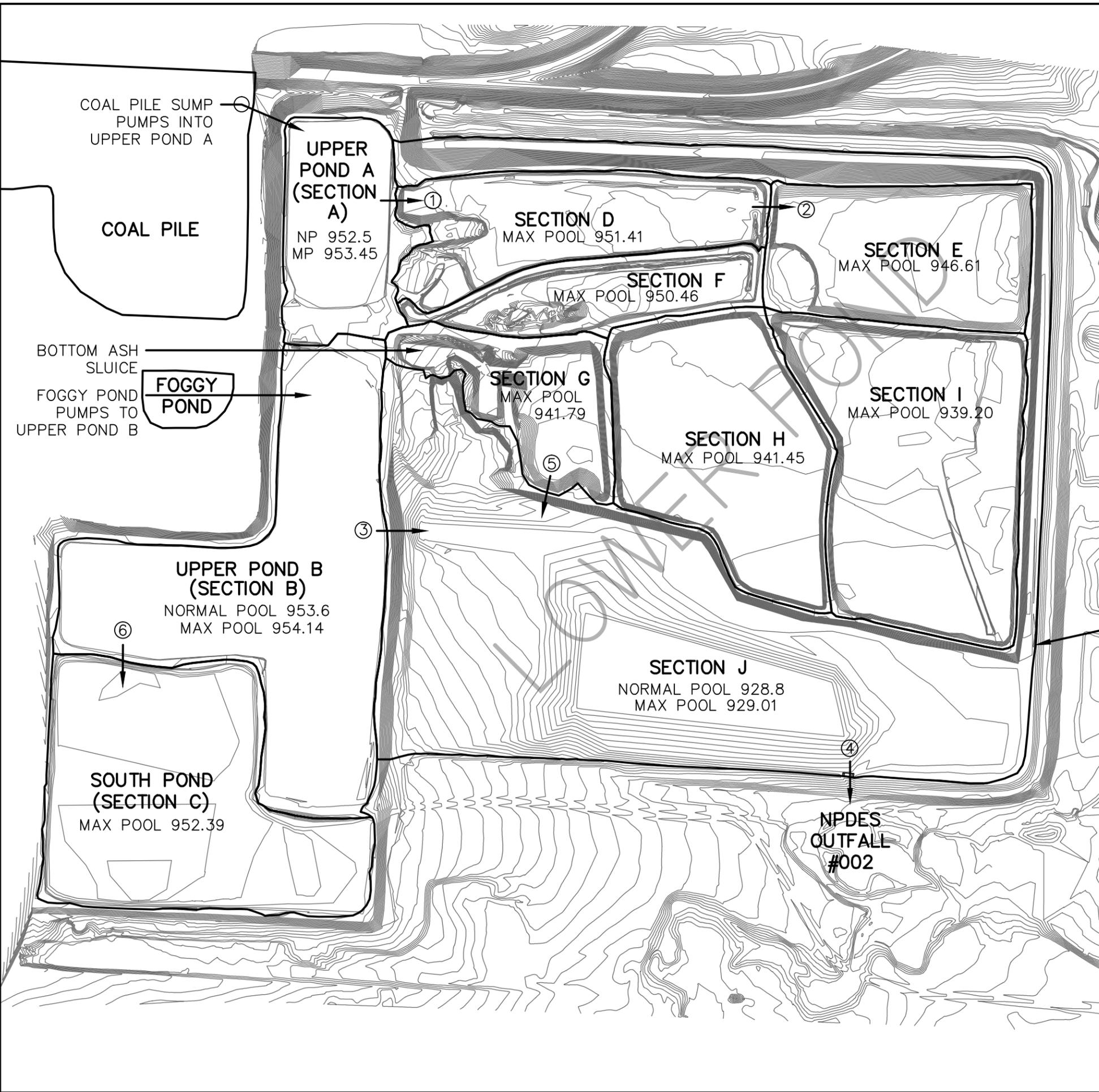
Site Location on 2013 Aerial Photograph

DATE: October 17, 2016

Project Number: 231518

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FIGURE 2



- ① 3-10" PIPES THROUGH DIKE
- ② 2-10" PIPES THROUGH DIKE
- ③ 1-10" PIPE THROUGH DIKE
- ④ NPDES OUTFALL #002
PRIMARY SPILLWAY: 2-12" PIPES WITH VALVES THROUGH DIKE
AUXILIARY SPILLWAY: 24' WIDE CONCRETE SPILLWAY ON TOP OF DIKE
- ⑤ 3-12" PIPES THROUGH DIKE
- ⑥ 2-12" PIPES WITH VALVES THROUGH DIKE

SECTION DRAINAGE AREA BOUNDARY



SCALE
1" = 300'

| | |
|--|------------------------|
| Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, Missouri | |
| Client: Empire District Electric Company | |
| Asbury CCR Impoundment | |
| DATE: October 17, 2016 | Project Number: 231518 |
| PPI PALMERTON & PARRISH, INC. | |
| GEOTECHNICAL AND MATERIALS ENGINEERS / MATERIALS TESTING LABORATORIES / ENVIRONMENTAL SERVICES | |
| FIGURE 3 | |

APPENDIX II
PRECIPITATION TABLE & PIPE FLOW CALCULATIONS



NOAA Atlas 14, Volume 8, Version 2
Location name: Asbury, Missouri, USA*
Latitude: 37.3608°, Longitude: -94.5889°
Elevation: 941.17 ft**
 * source: ESRI Maps
 ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk,
 Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF_tabular](#) | [PF_graphical](#) | [Maps & aeriels](#)

PF tabular

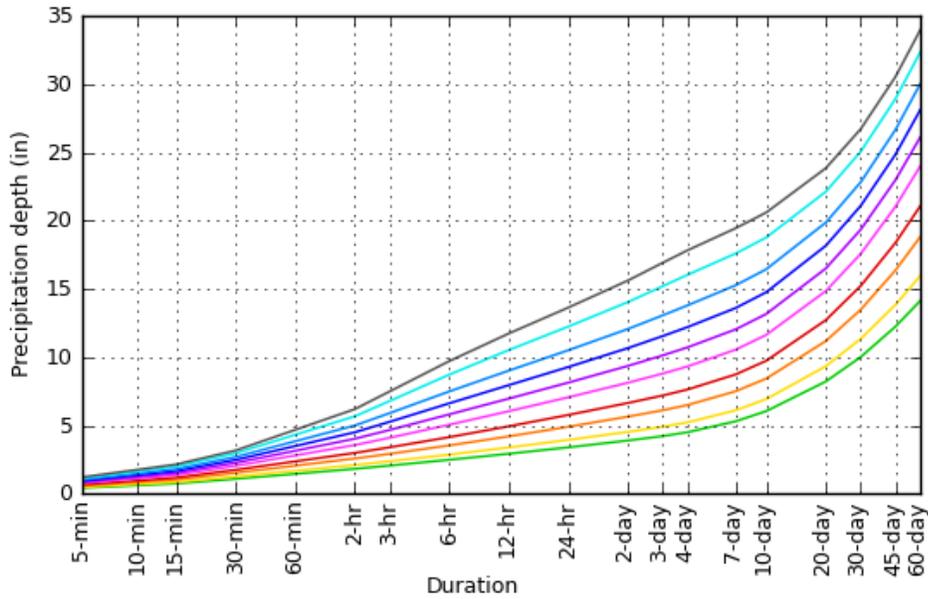
| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹ | | | | | | | | | | |
|--|--|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------|------------------------------|-----------------------------|-----------------------------|-----------------------------|
| Duration | Average recurrence interval (years) | | | | | | | | | |
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.415 (0.326-0.517) | 0.476 (0.374-0.594) | 0.575 (0.451-0.720) | 0.657 (0.513-0.824) | 0.767 (0.582-0.981) | 0.850 (0.634-1.10) | 0.932 (0.678-1.23) | 1.01 (0.715-1.36) | 1.12 (0.767-1.54) | 1.20 (0.806-1.67) |
| 10-min | 0.607 (0.478-0.758) | 0.697 (0.548-0.870) | 0.843 (0.661-1.05) | 0.961 (0.751-1.21) | 1.12 (0.852-1.44) | 1.25 (0.929-1.61) | 1.36 (0.993-1.80) | 1.49 (1.05-2.00) | 1.64 (1.12-2.25) | 1.76 (1.18-2.45) |
| 15-min | 0.741 (0.583-0.924) | 0.850 (0.669-1.06) | 1.03 (0.806-1.28) | 1.17 (0.916-1.47) | 1.37 (1.04-1.75) | 1.52 (1.13-1.96) | 1.67 (1.21-2.19) | 1.81 (1.28-2.44) | 2.00 (1.37-2.75) | 2.15 (1.44-2.99) |
| 30-min | 1.08 (0.854-1.35) | 1.25 (0.987-1.57) | 1.53 (1.20-1.91) | 1.75 (1.36-2.19) | 2.04 (1.55-2.61) | 2.26 (1.69-2.92) | 2.48 (1.80-3.26) | 2.69 (1.90-3.62) | 2.97 (2.02-4.07) | 3.17 (2.12-4.41) |
| 60-min | 1.45 (1.14-1.81) | 1.68 (1.32-2.10) | 2.05 (1.61-2.57) | 2.37 (1.85-2.97) | 2.80 (2.13-3.60) | 3.14 (2.35-4.08) | 3.49 (2.54-4.61) | 3.84 (2.71-5.18) | 4.32 (2.95-5.94) | 4.68 (3.14-6.52) |
| 2-hr | 1.82 (1.45-2.25) | 2.10 (1.67-2.60) | 2.58 (2.04-3.19) | 2.98 (2.35-3.71) | 3.56 (2.75-4.55) | 4.02 (3.04-5.19) | 4.50 (3.31-5.91) | 4.99 (3.56-6.70) | 5.67 (3.91-7.76) | 6.19 (4.18-8.57) |
| 3-hr | 2.06 (1.65-2.53) | 2.37 (1.90-2.92) | 2.92 (2.33-3.59) | 3.40 (2.69-4.20) | 4.09 (3.18-5.23) | 4.67 (3.55-6.01) | 5.26 (3.90-6.91) | 5.90 (4.23-7.91) | 6.79 (4.71-9.28) | 7.49 (5.08-10.3) |
| 6-hr | 2.48 (2.01-3.02) | 2.86 (2.31-3.48) | 3.53 (2.85-4.31) | 4.14 (3.32-5.07) | 5.05 (3.98-6.42) | 5.81 (4.47-7.44) | 6.62 (4.96-8.64) | 7.49 (5.42-9.98) | 8.72 (6.11-11.9) | 9.71 (6.63-13.3) |
| 12-hr | 2.92 (2.39-3.52) | 3.38 (2.76-4.08) | 4.20 (3.42-5.07) | 4.93 (4.00-5.98) | 6.04 (4.81-7.61) | 6.96 (5.42-8.85) | 7.95 (6.01-10.3) | 9.01 (6.58-11.9) | 10.5 (7.43-14.2) | 11.7 (8.07-16.0) |
| 24-hr | 3.39 (2.80-4.04) | 3.94 (3.25-4.70) | 4.90 (4.04-5.86) | 5.77 (4.73-6.92) | 7.06 (5.67-8.81) | 8.13 (6.39-10.2) | 9.28 (7.07-11.9) | 10.5 (7.73-13.8) | 12.2 (8.70-16.4) | 13.6 (9.44-18.4) |
| 2-day | 3.89 (3.25-4.59) | 4.53 (3.78-5.35) | 5.64 (4.70-6.68) | 6.64 (5.50-7.89) | 8.13 (6.59-10.0) | 9.36 (7.42-11.7) | 10.7 (8.20-13.6) | 12.1 (8.94-15.7) | 14.0 (10.0-18.7) | 15.6 (10.9-21.0) |
| 3-day | 4.22 (3.55-4.95) | 4.90 (4.12-5.76) | 6.11 (5.12-7.19) | 7.19 (5.99-8.49) | 8.80 (7.18-10.8) | 10.1 (8.07-12.6) | 11.5 (8.93-14.6) | 13.1 (9.73-16.9) | 15.2 (10.9-20.2) | 16.9 (11.8-22.6) |
| 4-day | 4.50 (3.80-5.26) | 5.22 (4.41-6.11) | 6.49 (5.46-7.61) | 7.63 (6.39-8.98) | 9.32 (7.63-11.4) | 10.7 (8.57-13.2) | 12.2 (9.47-15.4) | 13.8 (10.3-17.8) | 16.0 (11.6-21.2) | 17.8 (12.5-23.8) |
| 7-day | 5.30 (4.52-6.14) | 6.10 (5.20-7.08) | 7.50 (6.37-8.72) | 8.73 (7.38-10.2) | 10.5 (8.70-12.8) | 12.0 (9.70-14.7) | 13.6 (10.6-17.0) | 15.3 (11.5-19.6) | 17.6 (12.8-23.1) | 19.4 (13.7-25.8) |
| 10-day | 6.04 (5.18-6.97) | 6.92 (5.93-7.99) | 8.43 (7.20-9.74) | 9.74 (8.27-11.3) | 11.6 (9.63-14.0) | 13.2 (10.6-16.0) | 14.8 (11.6-18.4) | 16.4 (12.4-21.0) | 18.8 (13.7-24.5) | 20.6 (14.6-27.2) |
| 20-day | 8.21 (7.13-9.37) | 9.34 (8.09-10.7) | 11.2 (9.65-12.8) | 12.7 (10.9-14.6) | 14.8 (12.4-17.5) | 16.5 (13.4-19.8) | 18.2 (14.3-22.3) | 19.9 (15.1-25.0) | 22.1 (16.2-28.6) | 23.8 (17.0-31.3) |
| 30-day | 10.0 (8.74-11.3) | 11.3 (9.89-12.9) | 13.5 (11.7-15.3) | 15.2 (13.2-17.4) | 17.6 (14.7-20.6) | 19.3 (15.8-23.0) | 21.1 (16.7-25.6) | 22.8 (17.4-28.5) | 25.0 (18.4-32.2) | 26.7 (19.1-34.9) |
| 45-day | 12.2 (10.8-13.8) | 13.8 (12.2-15.6) | 16.4 (14.3-18.5) | 18.4 (16.0-20.9) | 21.0 (17.6-24.4) | 23.0 (18.9-27.1) | 24.8 (19.8-30.0) | 26.7 (20.4-33.1) | 28.9 (21.3-36.9) | 30.5 (22.0-39.8) |
| 60-day | 14.1 (12.5-15.8) | 15.9 (14.1-17.9) | 18.8 (16.5-21.2) | 21.1 (18.4-23.8) | 24.0 (20.2-27.7) | 26.1 (21.5-30.6) | 28.1 (22.4-33.8) | 30.0 (23.0-37.1) | 32.3 (23.9-41.1) | 34.0 (24.5-44.1) |

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

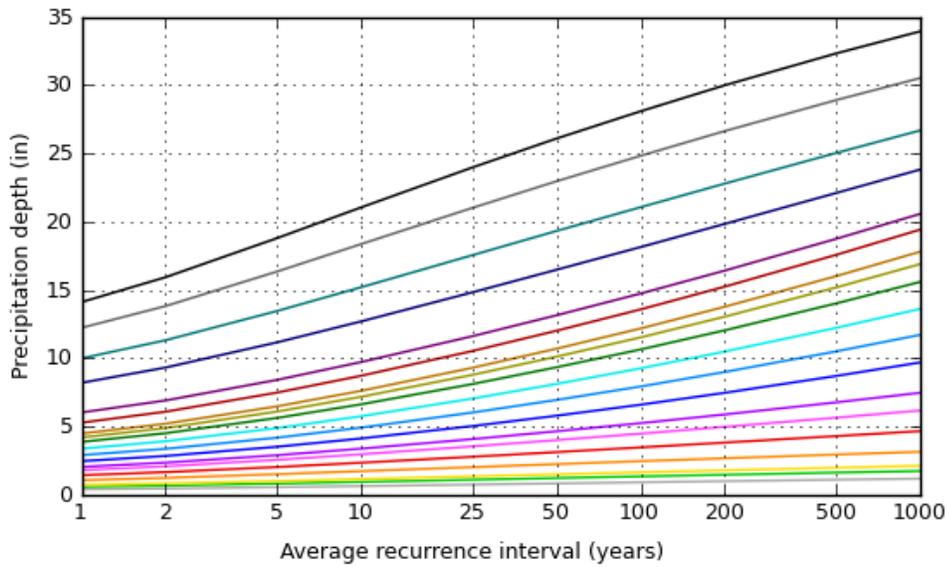
[Back to Top](#)

PF graphical

PDS-based depth-duration-frequency (DDF) curves
 Latitude: 37.3608°, Longitude: -94.5889°



| Average recurrence interval (years) |
|-------------------------------------|
| 1 |
| 2 |
| 5 |
| 10 |
| 25 |
| 50 |
| 100 |
| 200 |
| 500 |
| 1000 |

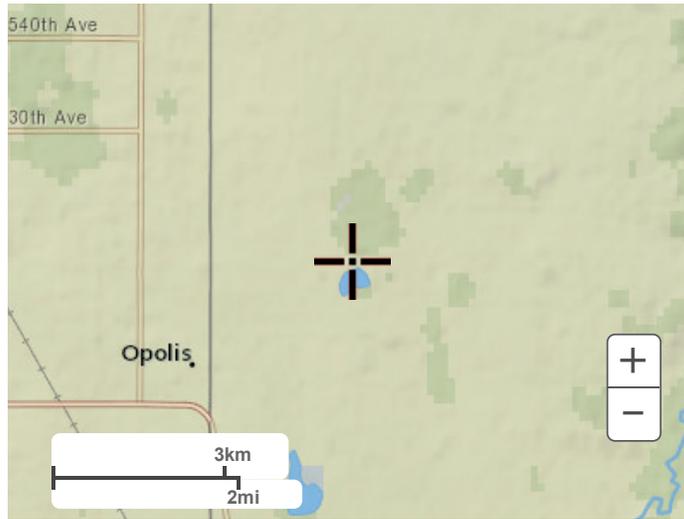


| Duration | |
|----------|--------|
| 5-min | 2-day |
| 10-min | 3-day |
| 15-min | 4-day |
| 30-min | 7-day |
| 60-min | 10-day |
| 2-hr | 20-day |
| 3-hr | 30-day |
| 6-hr | 45-day |
| 12-hr | 60-day |
| 24-hr | |

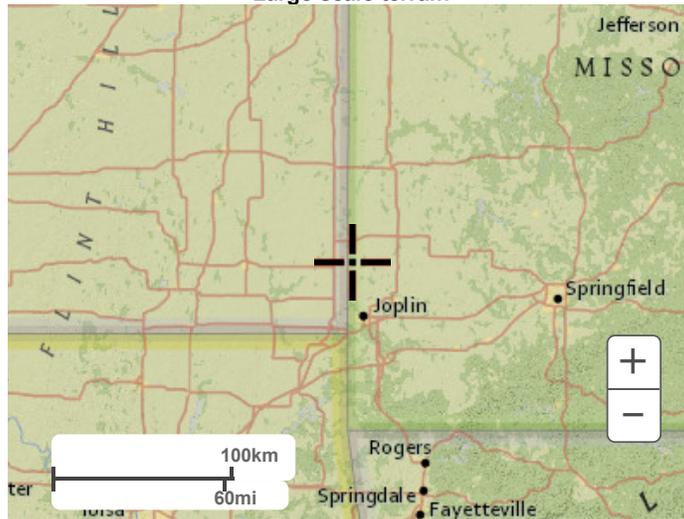
[Back to Top](#)

Maps & aerials

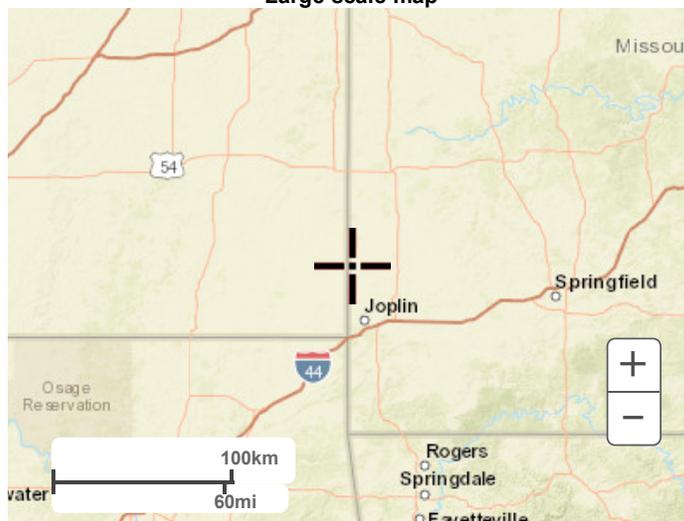
Small scale terrain



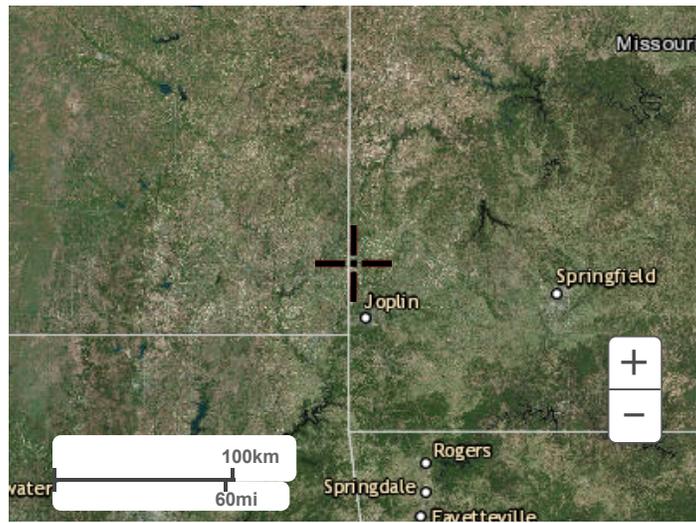
Large scale terrain



Large scale map



Large scale aerial



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[US Department of Commerce](#)
[National Oceanic and Atmospheric Administration](#)
[National Weather Service](#)
[National Water Center](#)
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

[Disclaimer](#)

Asbury CCR Impoundment - Pipe Flow Calculations

Manning's Equation $V = (Cf/n) R^{0.67} S^{0.5}$

$Q = VA$

V = Velocity (ft/sec) Cf = Conversion factor S = Slope

Q = Flow (cu ft/sec) n = Pipe roughness coefficient

R = Hydraulic Radius (ft) = Area (A) / Wetted Perimeter (P)

Upper Pond A to Section D

| | | |
|----------|-------|-------|
| Q | 5.82 | cfs |
| V | 10.68 | fps |
| Pipe Dia | 10 | in |
| | 0.83 | ft |
| n | 0.012 | PVC |
| Cf | 1.49 | |
| A | 0.55 | sq ft |
| P | 2.62 | ft |
| S | 0.06 | |
| R | 0.21 | ft |

Section D to Section E

| | | |
|----------|-------|-------|
| Q | 4.76 | cfs |
| V | 8.72 | fps |
| Pipe Dia | 10 | in |
| | 0.83 | ft |
| n | 0.012 | PVC |
| Cf | 1.49 | |
| A | 0.55 | sq ft |
| P | 2.62 | ft |
| S | 0.04 | |
| R | 0.21 | ft |

Section G to Lower Pond J

| | | |
|----------|-------|-------|
| Q | 11.21 | cfs |
| V | 14.27 | fps |
| Pipe Dia | 12 | in |
| | 1 | ft |
| n | 0.012 | PVC |
| Cf | 1.49 | |
| A | 0.79 | sq ft |
| P | 3.14 | ft |
| S | 0.084 | |
| R | 0.25 | ft |

Upper Pond B to Lower Pond J

| | | |
|----------|-------|-------|
| Q | 3.36 | cfs |
| V | 6.17 | fps |
| Pipe Dia | 10 | in |
| | 0.83 | ft |
| n | 0.012 | PVC |
| Cf | 1.49 | |
| A | 0.55 | sq ft |
| P | 2.62 | ft |
| S | 0.02 | |
| R | 0.21 | ft |

Outlet - Outfall 002

| | | |
|----------|-------|-------|
| Q | 5.47 | cfs |
| V | 6.97 | fps |
| Pipe Dia | 12 | in |
| | 1 | ft |
| n | 0.012 | PVC |
| Cf | 1.49 | |
| A | 0.79 | sq ft |
| P | 3.14 | ft |
| S | 0.02 | |
| R | 0.25 | ft |

Asbury CCR Impoundment - Pipe Flow Calculations

Hazen Williams Equation for Flow

$$Q = 0.285 C (D^{2.63})(S^{0.54})$$

Q = Flow (cu ft/sec)

C = Hazen Williams Friction Coefficient (140 for PVC)

D = Pipe Diameter (ft)

S = Hydraulic Grade Line Slope = Water Height/Pipe Length (50')

Pressure flow from 10" pipe between Section D and Section E.

| Water Height | S | Q | Water Elev |
|-----------------|------|-------|---------------|
| 2.5 | 0.05 | 4.895 | 951 |
| 3.5 | 0.07 | 5.870 | 952 |

APPENDIX III
HEC-1 OUTPUT

APPENDIX III-1

HEC-1 OUTPUT

UPPER POND A, SECTION D, & SECTION E

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1.1 *
* RUN DATE 12OCT16 TIME 10:12:46 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOB- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF "AMSK" ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUMMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: ADE.TXT
7 ID DATE: OCTOBER 17, 2016

Appendix III-1
Page 1 of 24

8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: UPPER POND A FLOWING INTO SECTIONS D AND E
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***NO OF INTERVALS*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
12 IT 1 1440
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
*DIAGRAM
* 1000-YR
15 JR PREC 13.60
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

16 KK UPA
17 RM COAL PILE AND UPPER POND A
18 PB 1.00
* DRAINAGE AREA: 24.08 ACRES = 0.0376 SQ. MI.
19 BA 0.0376
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505
35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997

Appendix III-1
Page 2 of 24

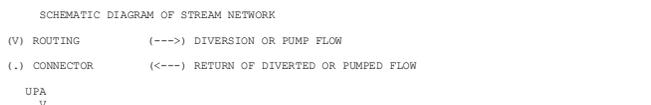
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
47 KK UPA
48 RM UPPER POND A
49 RS 1 ELEV 0953.0
50 SA 3.4086 3.5908
51 SE 953.0 954.0
52 SQ 11.640 17.460
53 SE 953.0 954.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 KK SECD
55 RM SECTION D
56 PB 1.00
* DRAINAGE AREA: 6.52 ACRES = 0.0102 SQ. MI.
57 BA 0.0102
* SCS CURVE NUMBER: 98.00
58 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
59 UD 0.0500
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
60 KK COMB
61 RM COMBINATION OF SUB BASINS
62 HC 2
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
63 KK BASND
64 RM BASIN IN SECTION D
65 RS 1 ELEV 0947.0

Appendix III-1
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66 SA 0.7216 1.9397 4.2220 4.7966 5.0074 5.1685
67 SE 947.0 948.0 949.0 950.0 951.0 952.0
68 SQ 0.0000 0.0000 9.50 9.52 9.79 11.74
69 SE 947.0 948.0 949.0 950.0 951.0 952.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

70 KK SECE
71 RM SECTION E
72 PB 1.00
* DRAINAGE AREA: 7.02 ACRES = 0.0110 SQ. MI.
73 BA 0.0110
* SCS CURVE NUMBER: 98.00
74 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
75 UD 0.0500
1 HEC-1 INPUT PAGE 3
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
76 KK COMB
77 RM COMBINATION OF SUB BASINS
78 HC 2
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
79 KK BASNE
80 RM BASIN IN SECTION E
81 RS 1 ELEV 0939.0
82 SA 0.0936 0.3554 0.8310 2.1810 4.4409 5.2631 5.4799 5.6485 5.8193 5.9915
83 SE 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0 948.0
84 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
85 SE 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0 948.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
86 ZZ



Appendix III-1
Page 4 of 24

Table with 10 columns of numerical data, likely representing hydrograph or routing parameters.

Table with 10 columns of numerical data, including parameters like SCS LOSS RATE and DIMENSIONLESS UNITGRAPH.

Table with 10 columns of numerical data, including routing data and storage-elevation characteristics.

Table with 10 columns of numerical data, including precipitation data and runoff characteristics.

Table with 10 columns of numerical data, mostly zeros, representing model output for Section D and Section E.

Table with 10 columns of numerical data, mostly zeros, representing model output for Section D and Section E.

Table with 10 columns of numerical data, including parameters like SCS LOSS RATE, SCS DIMENSIONLESS UNITGRAPH, and UNIT HYDROGRAPH ordinates.

Table with 10 columns of numerical data, including basin information (60 KK, 62 HC, 63 KK) and routing data (65 RS, 66 SA, 67 SE, 68 SQ, 69 SE).


```

75 UD      SCS DIMENSIONLESS UNITGRAPH
          TLAG          .05 LAG

          ***

          UNIT HYDROGRAPH
          17 END-OF-PERIOD ORDINATES
          69.  41.  26.
          16.  55.  88.  88.  17.  10.  6.
          4.   3.   2.   1.   1.   0.   0.

*****

*****
*         *
*   COMB   *
*         *
*****

          COMBINATION OF SUB BASINS

78 HC      HYDROGRAPH COMBINATION
          ICOMP        2 NUMBER OF HYDROGRAPHS TO COMBINE

          ***

*****

*****
*         *
*   BASNE  *
*         *
*****

          BASIN IN SECTION E

          HYDROGRAPH ROUTING DATA

81 RS      STORAGE ROUTING
          NSTPS        1 NUMBER OF SUBREACHES
          ITYP         ELEV TYPE OF INITIAL CONDITION
    
```

```

          UPA      .04  1  FLOW      14.
                   TIME      23.98

          ** PEAK STAGES IN FEET **
          1  STAGE      953.45
                   TIME      23.98

HYDROGRAPH AT
          SECD     .01  1  FLOW      4.
                   TIME      18.27

2 COMBINED AT
          COMB     .05  1  FLOW      18.
                   TIME      23.98

ROUTED TO
          BASND    .05  1  FLOW      11.
                   TIME      23.98

          ** PEAK STAGES IN FEET **
          1  STAGE      951.41
                   TIME      23.98

HYDROGRAPH AT
          SECE     .01  1  FLOW      4.
                   TIME      18.27

2 COMBINED AT
          COMB     .06  1  FLOW      15.
                   TIME      23.98

ROUTED TO
          BASNE    .06  1  FLOW      0.
                   TIME      .00

          ** PEAK STAGES IN FEET **
          1  STAGE      946.61
                   TIME      23.98
    
```

*** NORMAL END OF HEC-1 ***

```

          RSVRIC      939.00 INITIAL CONDITION
          X           .00 WORKING R AND D COEFFICIENT

82 SA      AREA      .1      .4      .8      2.2      4.4      5.3      5.5      5.6      5.8      6.0

83 SE      ELEVATION  939.00  940.00  941.00  942.00  943.00  944.00  945.00  946.00  947.00  948.00

84 SQ      DISCHARGE  0.      0.      0.      0.      0.      0.      0.      0.      0.      0.      0.

85 SE      ELEVATION  939.00  940.00  941.00  942.00  943.00  944.00  945.00  946.00  947.00  948.00

          ***

          COMPUTED STORAGE-ELEVATION DATA

          STORAGE     .00      .21      .79      2.24      5.48      10.33      15.70      21.27      27.00      32.90
          ELEVATION   939.00  940.00  941.00  942.00  943.00  944.00  945.00  946.00  947.00  948.00

          COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

          STORAGE     .00      .21      .79      2.24      5.48      10.33      15.70      21.27      27.00      32.90
          OUTFLOW     .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          ELEVATION   939.00  940.00  941.00  942.00  943.00  944.00  945.00  946.00  947.00  948.00
    
```

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

```

          RATIOS APPLIED TO PRECIPITATION
          RATIO 1
          13.60

OPERATION  STATION  AREA  PLAN  FLOW  TIME

HYDROGRAPH AT
          UPA      .04  1  FLOW  15.
                   TIME  21.22

ROUTED TO
    
```

**APPENDIX III-2
HEC-1 OUTPUT
LOWER POND C**

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 05OCT16 TIME 15:36:58 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOB- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSKX- ON RW-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: C.TXT

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: AREA C
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
12 IT
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
* DIAGRAM
* 1000-YR
15 JR PREC 13.60
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
16 KK SUBAC
17 RM SUB AREA C
18 PB 1.00
* DRAINAGE AREA: 12.40 ACRES = 0.0194 SQ. MI.
19 BA 0.0194
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507

1 HEC-1 INPUT PAGE 2
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500

47 KK BASNC
48 RM BASIN C
49 RS 1 ELEV 950.0
50 SA 0.5564 5.4486 9.2805 10.598 11.433 11.769
51 SE 950.0 0951.0 952.0 953.0 954.0 955.0
52 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 950.0 0951.0 952.0 953.0 954.0 955.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SUBAC
V
47 BASNC

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 05OCT16 TIME 15:36:58 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P.E.
FILE NAME: C.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: AREA C

14 IO OUTPUT CONTROL VARIABLES
IFRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

APPENDIX III-3
HEC-1 OUTPUT
SECTION F

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:37 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X XXXXXX XXXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIO- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSKX- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: F.TXT

Appendix III-3
Page 1 of 11

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: SECTION F
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-260 12-720 18-1080 24-1440
12 IT
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
*DIAGRAM
* 1000-YR
15 UR PREC 13.60
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

16 HK SECF
17 RM SECTION F
18 PB 1.00
* DRAINAGE AREA: 3.99 ACRES = 0.0062 SQ. MI.
19 BA 0.0062
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

Appendix III-3
Page 2 of 11

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507

1 HEC-1 INPUT PAGE 2
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
47 HK BASNF
48 RM BASIN SECTION F
49 RS 1 ELEV 946.0
50 SA 0.0814 0.3307 0.6452 1.5414 1.8699 2.3758 3.1287 3.3812
51 SE 946.0 0947.0 949.0 949.0 950.0 951.0 952.0 953.0
52 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 946.0 0947.0 948.0 949.0 950.0 951.0 952.0 953.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECF
V
47 BASNF

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

Appendix III-3
Page 3 of 11

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:37 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P.E.
FILE NAME: F.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION F

14 IO OUTPUT CONTROL VARIABLES
IFRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

Appendix III-3
Page 4 of 11

APPENDIX III-4
HEC-1 OUTPUT
SECTION G

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:47 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIO- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSKX- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: G.TXT

Appendix III-4
Page 1 of 11

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: SECTION G
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
12 IT *****
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
* DIAGRAM
* 1000-YR
15 UR PREC 13.60
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
16 HK SECG
17 RM SECTION G
18 PB 1.00
19 BA 0.0069
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

Appendix III-4
Page 2 of 11

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507

1 HEC-1 INPUT PAGE 2
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
47 HK BASNG
48 RM BASIN SECTION G
49 RS 1 ELEV 937.0
50 SA 0.0631 0.6902 1.2727 1.5650 1.7619 1.8770 2.1662 2.3247 2.4937 2.6722
51 SE 937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0
52 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECG
V
47 BASNG

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

Appendix III-4
Page 3 of 11

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:47 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P.E.
FILE NAME: G.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION G

14 IO OUTPUT CONTROL VARIABLES
IFRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

Appendix III-4
Page 4 of 11

APPENDIX III-5
HEC-1 OUTPUT
SECTION H

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:58 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X XXXXXXX XXXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIO- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSK- ON RW-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: H.TXT

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: SECTION H
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
12 IT *****
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
* DIAGRAM
* 1000-YR
15 JR PREC 13.60
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
16 KK SECH
17 RM SECTION H
18 PB 1.00
19 BA 0.0149
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
47 KK BASNH
48 RM BASIN SECTION H
49 RS 1 ELEV 939.0
50 SA 0.9156 3.4858 7.0104 8.2156 8.3012 8.3870 8.4735 8.5607 8.6486
51 SE 939.0 0940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0
52 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 939.0 0940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECH
V
47 BASNH

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:18:58 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P.E.
FILE NAME: H.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION H

14 IO OUTPUT CONTROL VARIABLES
IFRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

APPENDIX III-6
HEC-1 OUTPUT
SECTION I

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:19:08 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIO- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSKX- ON RW-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: I.TXT

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: SECTION I
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-260 12-720 18-1080 24-1440
12 IT
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
* DIAGRAM
* 1000-YR
15 UR PREC 13.60
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
16 HK SECI
17 RM SECTION I
18 PB 1.00
* DRAINAGE AREA: 12.19 ACRES = 0.0191 SQ. MI.
19 BA 0.0191
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
47 HK BASNI
48 RM BASIN SECTION I
49 RS 1 ELEV 936.0
50 SA 0.5474 3.1525 4.3224 8.4727 10.639 10.773 10.925 11.052 11.178 11.306
51 SE 936.0 0937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0
52 SQ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 936.0 0937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECI
V
47 BASNI

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11OCT16 TIME 14:19:08 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P.E.
FILE NAME: I.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION I

14 IO OUTPUT CONTROL VARIABLES
IFRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

APPENDIX III-7
HEC-1 OUTPUT
UPPER POND B & LOWER POND J

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 12OCT16 TIME 10:02:50 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF -RTIMP- AND -RTIO- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSKX- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID *****
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P.E.
6 ID FILE NAME: J.TXT

7 ID DATE: OCTOBER 17, 2016
8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: UPPER POND B AND LOWER POND J
11 ID *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
* ***No OF INTERVALS*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440

12 IT 1 1440
* *****
* NUMBER OF MIN IN EACH TIME INTERVAL
* ***MIN IN INTERVAL***1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
13 IN 72
14 IO 4 0
* *****
* 1000-YR
15 UR PREC 13.60
* *****
* STORM DISTRIBUTION: SCS TYPE II
* STORM DURATION: 24 HOUR
* *****
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

16 KK SECB
17 RM UPPER POND B
18 PB 1.00
* *****
* DRAINAGE AREA: 14.87 ACRES = 0.0232 SQ. MI.
19 BA 0.0232
* *****
* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
* SCS CURVE NUMBER: 98.00
45 LS 98.00
* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
46 UD 0.0500
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

47 KK FPOND
48 RM FOGGY POND DA
49 PB 1.00
* DRAINAGE AREA: 0.89 ACRES = 0.0005 SQ. MI.
50 BA 0.0005
* SCS CURVE NUMBER: 93.42
51 LS 93.42
* TIME OF CONCENTRATION: 0.2330 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
52 UD 0.0500
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

53 KK COMB KK
54 RM COMBINATION OF SUB BASINS RM
55 HC 2 HC
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
56 KK BASNB
57 RM BASIN UPPER POND B
58 RS 1 ELEV 927.0
59 SA 11.513 13.361 14.116
60 SE 953.6 954.0 955.0
61 SQ 0.0000 6.7200 6.7200
62 SE 953.6 954.0 955.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

63 KK SECB
64 RM LOWER POND J DA
65 PB 1.00
* DRAINAGE AREA: 39.30 ACRES = 0.0614 SQ. MI.
66 BA 0.0614
* SCS CURVE NUMBER: 82.31
67 LS 82.31
* TIME OF CONCENTRATION: 0.2330 HR (LAG TIME = 0.6 * Tc = 0.0500 HR)
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10

68 KK COMB KK
69 RM COMBINATION OF SUB BASINS RM
70 HC 2 HC
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 HEC-1 INPUT PAGE 3
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

71 KK BASNJ
72 RM BASIN LOWER POND J
73 RS 1 ELEV 927.0
74 SA 9.3025 9.5541 13.442 17.103
75 SE 928.8 929.0 930.0 931.0
76 SQ 0.0000 6.700 10.940 60.240
77 SE 928.8 929.0 930.0 931.0
*1.....2.....3.....4.....5.....6.....7.....8.....9.....10
78 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECB
.
.
47 . FPOND
.
53 COMB.....

Table with 10 columns of numerical data, mostly zeros, representing model output for various parameters.

Table with 10 columns of numerical data, including text labels like 'SCS LOSS RATE', 'INITIAL ABSTRACTION', and 'UNIT HYDROGRAPH'.

Table with 10 columns of numerical data, including text labels like '47 KK', 'FOGGY POND DA', 'SUBBASIN RINOFF DATA', 'SUBBASIN CHARACTERISTICS', 'PRECIPITATION DATA', and 'INCREMENTAL PRECIPITATION PATTERN'.

Table with 10 columns of numerical data, including text labels like '49 FB', '19 PI', and '17 END-OF-PERIOD ORDINATES'.

Table with 10 columns of numerical data, mostly zeros, representing model output for Appendix III-7.

Table with 10 columns of numerical data, including parameters like SCS LOSS RATE and SCS DIMENSIONLESS UNITGRAPH, representing model output for Appendix III-7.

Table with 10 columns of numerical data, including parameters like HYDROGRAPH COMBINATION and STORAGE ROUTING, representing model output for Appendix III-7.

Table with 10 columns of numerical data, including parameters like ELEVATION, STORAGE, and SUBBASIN CHARACTERISTICS, representing model output for Appendix III-7.

Table with 10 columns of numerical data, all values are .00.

Table with 10 columns of numerical data, all values are .00.

Table with 10 columns of numerical data, all values are .00.

Table with 10 columns of numerical data and text. Includes parameters like SCS LOSS RATE, INITIAL ABSTRACTION, and HYDROGRAPH COMBINATION.

```

*****
      BASIN LOWER POND J
HYDROGRAPH ROUTING DATA
73 RS  STORAGE ROUTING
      NSTPS      1  NUMBER OF SUBREACHES
      ITYP      ELEV  TYPE OF INITIAL CONDITION
      RSVRIC    927.00 INITIAL CONDITION
      X         .00 WORKING R AND D COEFFICIENT
74 SA  AREA      9.3    9.6    13.4   17.1
75 SE  ELEVATION 928.80 929.00 930.00 931.00
76 SQ  DISCHARGE 0.     7.     11.    60.
77 SE  ELEVATION 928.80 929.00 930.00 931.00
      ***
      COMPUTED STORAGE-ELEVATION DATA
      STORAGE .00  1.89  13.33  28.56
      ELEVATION 928.80 929.00 930.00 931.00
      COMPUTED STORAGE-OUTFLOW-ELEVATION DATA
      STORAGE .00  1.89  13.33  28.56
      OUTFLOW .00  6.70  10.94  60.24
      ELEVATION 928.80 929.00 930.00 931.00
1
      PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
      FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
      TIME TO PEAK IN HOURS
      RATIOS APPLIED TO PRECIPITATION
OPERATION STATION AREA PLAN RATIO 1
HYDROGRAPH AT SECB .02 1 FLOW 9.

```

```

      TIME 20.68
HYDROGRAPH AT FPOND .00 1 FLOW 0.
      TIME 15.83
2 COMBINED AT COMB .02 1 FLOW 9.
      TIME 23.28
ROUTED TO BASNB .02 1 FLOW 7.
      TIME 14.70
      ** PEAK STAGES IN FEET **
      1 STAGE 954.14
      TIME 23.98
HYDROGRAPH AT SECJ .06 1 FLOW 0.
      TIME 22.30
2 COMBINED AT COMB .09 1 FLOW 7.
      TIME 22.30
ROUTED TO BASNJ .09 1 FLOW 7.
      TIME 23.87
      ** PEAK STAGES IN FEET **
      1 STAGE 929.01
      TIME 23.95
*** NORMAL END OF HEC-1 ***

```